

Notes by-

Pravin S Kolhe,

BE(Civil), Gold Medal, MTech (IIT-K)

Assistant Executive Engineer,

Water Resources Department,

www.pravinkolhe.com

Open Channel Flows

Questions of Examination :- Q 10(a) Sketch the specific energy diagram for a constant flow through open channel. (5). 10(b) Explain the principle and working of current meter (5).

(1992) Q.8 Design a concrete lined trapezoidal channel section to carry a discharge of $200 \text{ m}^3/\text{s}$ through a terrain where the longitudinal slope is 0.004. Assume side slopes of 1:1 and take Manning's n as 0.14 for design. Draw a sketch of the section with usual details needed for a canal. Use formula $B = 0.7\sqrt{Q}$ for bottom width. (15) (1981) : (7c) 20 m^3/s of water flows through a 6m wide rectangular channel at a velocity of 2 m/s . Calculate the sp. energy of flowing water. Also calculate minimum sp. energy and critical depth for this discharge. (4)

Q.9 Sketch the water surface profile in a long rectangular channel for the following two situations. (i) the bed slope changes from mild to steep (ii) the bed slope changes from steep to mild. (6) (9b) A wide rectangular channel carries a discharge of $3 \text{ m}^3/\text{s}$ per m width of channel. It has a bed slope of 1:10,000. If at a section in this channel the depth is 1.6m how far upstream or downstream from this section will the depth be 2.0m? Assume Manning's $n = 0.015$. (9) (1999) 3(a) (i) Explain the hydraulically efficient channel section. Derive the conditions for a most efficient trapezoidal section in open channel flows. (ii) Distinguish between sp. energy and sp. force in an open channel. (5) (1b) A river 45m wide has a normal depth of flow of 4m and average bed slope of 1:12000. A weir is built across the river raising the water surface level at the weir site to 5.5m above the bottom of the river. Assuming that the backwater curve is an arc of a circle, calculate the approximate length of the back water curve. Consider that the river is prismatic. Take the value of n in Manning's formula as 0.025. (10) 1996 3(c) What are M_1 & M_2 curves in an open channel? Discuss the condition under which they occur. (10) (3b) A hydraulic jump occurs in a rectangular channel. The details are as follows. (1) Width of channel = 5m, Discharge = $5 \text{ m}^3/\text{s}$, Depth of water before jump = 0.2m. Find (1) Froude numbers before jump. (2) Depth after jump (3) Froude number after jump (4) Length of jump (5) Height of jump. (10)

1) * Determine the efficient section of a trapezoidal channel with side slopes 1:2 carrying a discharge of $11.25 \text{ m}^3/\text{s}$ with a velocity of 0.75 m/s . What should be the bed slope of the channel? $n = 0.025$ $y = 2.46 \text{ m}; B = 1.16 \text{ m}; S_o = 0.0001$

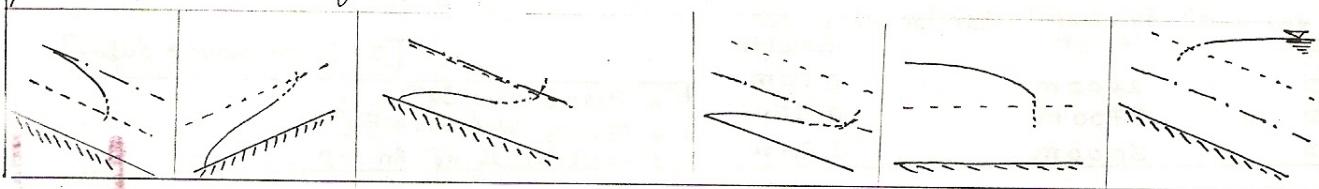
2) Uniform flow occurs at a depth of 1.5m in a long rectangular channel 3m wide and laid at a slope of 0.0009. If the Manning's n is given as 0.015, calculate the width of contraction which will produce critical depth without increasing the depth of flow. [2.08m]

3) A rectangular channel 10m wide carries a discharge of $40 \text{ m}^3/\text{s}$. If at a section in this channel the depth is 1.5m, how far upstream or downstream from this section will the depth be 2.0m? Take $S_o = 0.00009$ and $n = 0.017$ [3.67m upstream]

4) A rectangular channel carries a discharge of $3 \text{ m}^3/\text{s}$ per m width. If the loss of energy in the hydraulic jump is found to be 3.2m, determine the conjugate depths before and after the jump. [Hint: $\Delta E = (y_2 - y_1)^3 / 4y_1 y_2$ & $y_2/y_1 = \frac{1}{2}(1 + \sqrt{1 - 8F})$] Solve by trial & error Ans: [0.293m, 2.36m]

5) A rectangular channel 4.5m wide carries 12 m^3 of water per second with a velocity of 1.5 m/s . Compute the sp. energy. Also find the depth of flow in the channel when the sp. energy would be minimum. What will be the value of critical velocity as well as minimum sp. energy. [1.18m, 0.639m, 2.503 m/s , 0.459m]

6) Identify the flow profiles :-



Open channel Flow

Er. Pravin Kolhe
(B.E Civil)

25/01/04

①

Pro: Design a concrete lined trapezoidal channel of section to carry a discharge of $200 \text{ m}^3/\text{s}$ through a terrain where the longitudinal slope is 0.004. Assume side slopes of 1:1 & take manning $n=0.14$. for design. Draw a sketch of the section with usual details needed for a channel. Use formula, $B = 0.7\sqrt{Q}$ for water bottom width. (15M) 1992

$$\text{Soln: } Q = 200 \text{ m}^3/\text{s}$$

$$S = 0.004$$

$Z = 1:1 = 1$ Horizontal.

$$n = 0.14$$

$$B = 0.7\sqrt{Q}$$

$$Q = \frac{1}{n} \cdot A \cdot R^{2/3} \cdot S^{1/2}$$

Max. per. vel. for concrete channel = 6 m/s.

Min. per. vel. for = 3 m/s.

$$\therefore V = \frac{1}{n} \cdot R^{2/3} \cdot S^{1/2}$$

$$\therefore 6 = \frac{1}{0.14} \times R^{2/3} \times \sqrt{0.004}$$

$$\therefore R = 48.4 \text{ m}$$

$$\text{But } R = \frac{A}{P}$$

$$Q = A \cdot V \Rightarrow A = \frac{Q}{V} = \frac{2000}{6} = 33.33 \text{ m}^2$$

$$\therefore P = \frac{A}{R} = \frac{48.4}{33.33} = 1.452 \text{ m} \quad 0.69 \text{ m}$$

$$P = B + \sqrt{Z^2 + 1} \quad (2y)$$

$$\therefore 0.69 = B + 2\sqrt{2} \times 0.4y \quad (2y) \Rightarrow B + 2.828y = 0.69$$

$$A = B + 2y$$

$$\therefore 33.33 = B + 2y$$

$$\therefore B = 112.12$$

$$B = 0.7\sqrt{Q}$$

$$= 0.7 \times \sqrt{200} = 9.899 \text{ m}$$

$$\therefore B = 9.899 \text{ m}$$

Ques: 20 m³/s of water flows through a 6m wide rectangular channel at a velocity of 2m/s. calculate the specific energy of flowing water. Also, calculate min. sp. energy & critical depth for this discharge.

Sol: - $Q = 20 \text{ m}^3/\text{s}$
 $B = 6 \text{ m}$, $R = y$
 $V = 2 \text{ m/s}$

calculate

E,

$$E_{\min} = E_c$$

y_c

$$E = y + \frac{Q^2}{2gA^2}$$

$$\textcircled{1} Q = A \cdot V$$

$$\therefore A = \frac{Q}{V} = \frac{20}{2} = 10 \text{ m}^2$$

$$\therefore 6 \times y = 10 \text{ m}^2$$

$$\boxed{\therefore y = 1.67 \text{ m}}$$

$$\textcircled{2} E = y + \frac{Q^2}{2g(A^2)}$$

$$= 1.67 + \frac{20^2}{2 \times 9.81 \times (6 \times 1.67)^2}$$

$$\boxed{E = 1.87}$$

$$\textcircled{3} y_c = \left(\frac{Q^2}{g} \right)^{1/3}$$

$$= \left[\frac{(Q/B)^2}{g} \right]^{1/3}$$

$$= \left(\frac{(20/6)^2}{9.81} \right)^{1/3}$$

$$\boxed{y_c = 0.698 \text{ m}}$$

$$\boxed{y_c = 1.042 \text{ m}}$$

$$\textcircled{4} E_c = \frac{3}{2} y_c$$

$$\boxed{E_c = 1.0467}$$

$$\boxed{E_c = 1.563}$$

Ques:- A hydraulic jump occurs in a rectangular channel. The (2)

details are as follows :-

① Width of channel = 5m

② Discharge = 5 m³/s

③ Depth of water before jump = 0.2m

(A) find -

① Fr. No. Before jump

② Depth after jump

③

Soln:- $B = 5\text{m}$
 $Q = 5\text{ m}^3/\text{s}$
 $y_1 = 0.2\text{m}$

$$\begin{aligned} F_1 &= \frac{V}{\sqrt{gD}} \\ &= \frac{Q}{\sqrt{g \cdot (A/T)} \times A} \\ &= \frac{5}{\sqrt{9.81 \times (5 \times 0.2)}} \times 5 \times 0.2 \end{aligned}$$

$$F_1 = 3.57$$

$$\frac{y_2}{y_1} = \frac{1}{2} (-1 + \sqrt{1 + 8F_1^2})$$

$$y_2 = \frac{0.2}{2} \left(-1 + \sqrt{1 + 8 \times 3.57^2} \right)$$

$$y_2 = 0.91\text{m}$$

$$y_2 = 0.91\text{m}$$

$$F_2 = \frac{Q/A}{\sqrt{g \cdot (A/T)}}$$

$$= \frac{5 / (5 \times 0.91)}{\sqrt{9.81 \times 5 \times 0.91}} \times 5$$

$$F_2 = 0.368\text{m}$$

$$\therefore F_1 = 3.57, F_2 = 0.37 < 1 \quad \therefore \text{O.K.}$$

$$0.0 - 10.0 =$$

$$10.0 - 10.0 =$$

10.0 - 9.0 = 10.0

9.0 - 8.0 = 10.0

8.0 - 7.0 = 10.0

7.0 - 6.0 = 10.0

6.0 - 5.0 = 10.0

5.0 - 4.0 = 10.0

4.0 - 3.0 = 10.0

3.0 - 2.0 = 10.0

2.0 - 1.0 = 10.0

1.0 - 0.0 = 10.0

0.0 - 0.0 = 10.0

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$$\text{HT of jump} = y_2 - y_1 \\ = 0.91 - 0.2 \\ = 0.71 \text{ m}$$

$$\text{Length of jump} = 5 h_j \\ = 5 \times 0.71 \\ = 3.55 \text{ m}$$

g(b)
[98]

[STEP BY STEP MTD]

Ques: A wide rectangular channel carries a discharge of $3 \text{ m}^3/\text{s}$ per m width of channel. It has a bed slope as $1:10000$. If at a section in this channel, the depth is 1.6 m how far upstream from this section will the depth be 2 m.

Assume $n = 0.015$

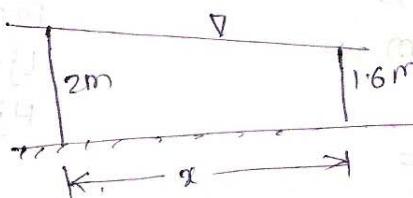
$$\text{Soln: } Q = 3 \text{ m}^3/\text{s}$$

$$S = \frac{1}{10000} = 10^{-4}$$

$$y_1 = 1.6 \text{ m}$$

$$y_2 = 2 \text{ m}$$

$$n = 0.015$$



Assume $B = 1 \text{ m}$.

$$V = \frac{1}{n} \cdot R^{2/3} \cdot S^{1/2}$$

Depth y	Area A (Bxy)	Perimeter P ($B+2y$)	Hydro. mean Radius (A/P)	Velocity V	$\frac{V^2}{2g}$	E	ΔE $E_1 - E_2$	Sf	\bar{Sf}	$S_0 - \bar{Sf}$	Δx
1.6 m	1.6	4.2	0.38	0.356	6.23×10^{-3} 0.01598	1.61598 1.6062	-	1.0016×10^{-4}	-	-	-
1.7 m	1.7	4.4	0.386	0.3539	6.3665×10^{-3}	1.7064	0.10016	9.998×10^{-5}	1.0006×10^{-4}	6.223×10^{-8}	160942×10^{-5}
1.8 m	1.8	4.6	0.3913	0.3566	6.4833×10^{-3}	1.8064	0.10008	9.9975×10^{-5}	9.9975×10^{-5}	2.4948×10^{-5}	39250×5
1.9 m											
2.0 m											

$$V = \frac{1}{n} \cdot R^{2/3} \cdot S^{1/2}$$

$$Sf = \left[\frac{V \cdot n}{R^{2/3}} \right]^2$$

$$Sf_1 = 1.0016 \times 10^{-4}$$

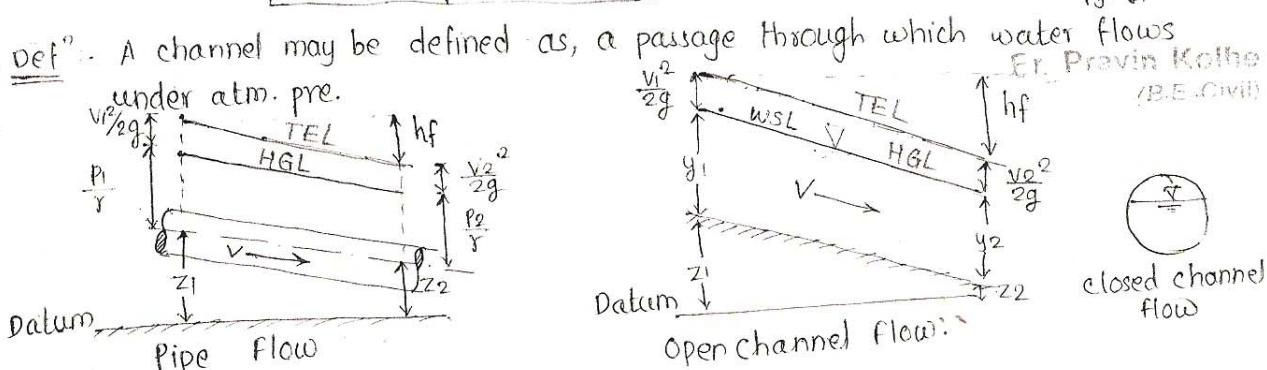
$$\bar{Sf} = \frac{Sf_1 + Sf_2}{2}$$

$$\Delta x = \frac{\Delta F}{S_0 - \bar{Sf}}$$

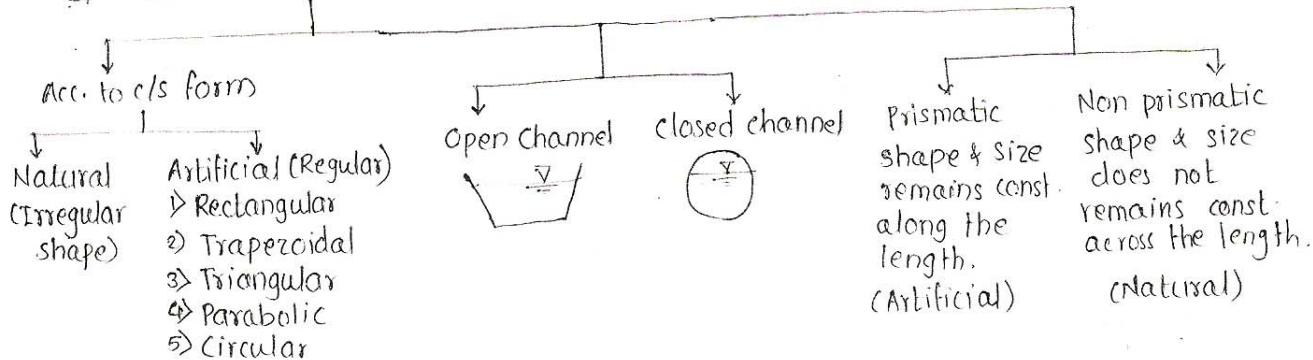
$$y_c = \left(\frac{q^2}{g} \right)^{1/3}$$

$$y_n = \left(\frac{q \cdot r}{\sqrt{Sf}} \right)^{3/5}$$

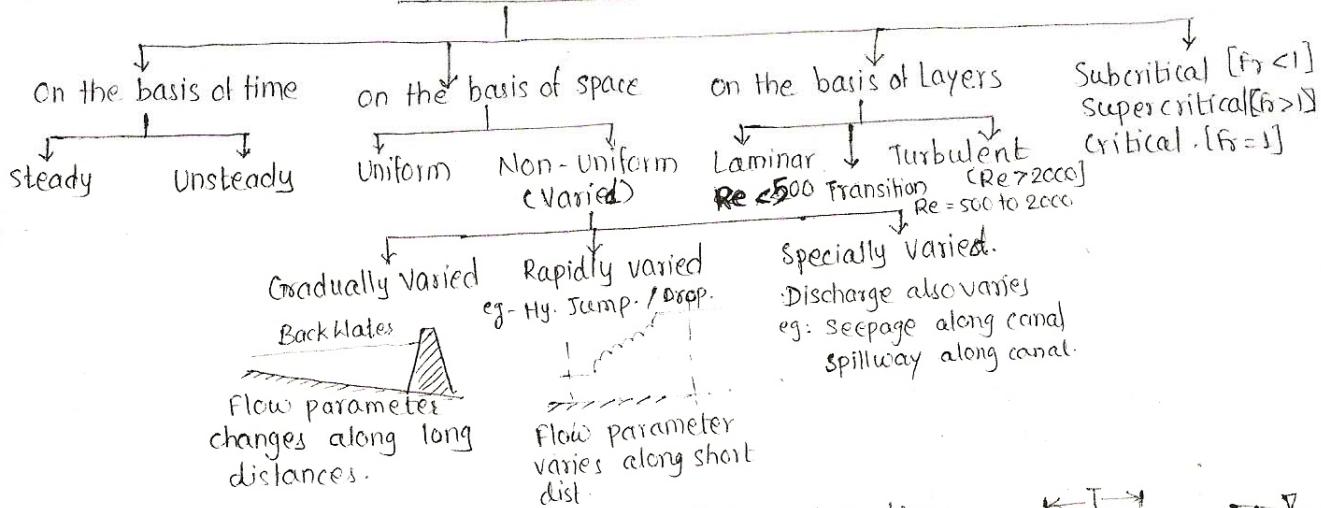
If $y_n > y_c \Rightarrow$ mild sloping channel
 $y > y_n > y_c \Rightarrow M_1$ profile



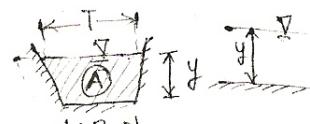
* Types of channels:-



Types of flow



Geometrical Properties of channel section:-

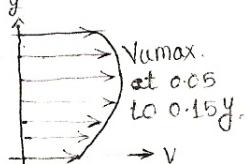
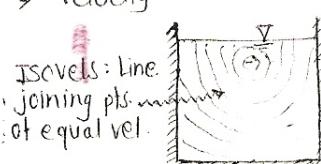


- 1) y = Depth of flow: Vertical dist from WSL to channel bed
- 2) T = Top width: Width of channel sectⁿ at the free surface
- 3) A = Wetted Area: c/s area normal to the flow directⁿ (Hatched)
- 4) P = Wetted Perimeter: length of channel boundary in contact with the flowing water at any section
- 5) B = Bottom width: Width across the channel at bed level
- 6) R = Hydraulic Mean Radius = A/P = (Wetted area)/(Wetted perimeter)
- 7) D = Hydraulic mean depth = A/T = (Wetted area)/(Top width)
- 8) Z = Section factor:

$$\text{for critical flow, } Z = A\sqrt{D} = A\sqrt{(A/T)} = \sqrt{A^3/T}$$

$$\text{for Uniform flow, } Z = AR^{2/3}$$

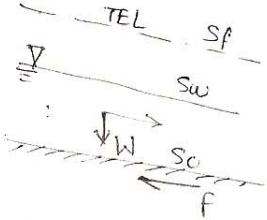
Velocity Distribution in channel section:-



10) α = Kinetic Energy correction factor (Lemo Coriolis coeff.) \rightarrow (1.03 to 1.36)

11) β = Momentum correction factor (Boussinesq coeff) \rightarrow (1.01 to 1.12)

Uniform flow : $S_0 = S_w = S_f$ & Gravitational forces = Resisting force.



* Uniform Flow formulae:-

$$① \text{Chezy's Eqn} : V = C \sqrt{R S_f} = C \cdot \sqrt{R S_0} \Rightarrow C = \sqrt{\frac{8g}{f}} \text{ where } f = \text{friction factor.}$$

$$② \text{Mannings Eqn} : V = \frac{1}{n} R^{2/3} S_0^{1/2}$$

$$③ \text{Relation b/w } C \text{ & } n : C = \frac{1}{n} R^{1/6}$$

$$④ \text{Sticklers Eqn} : n = \frac{d_{50}}{24} \rightarrow d_{50} = \text{Mean particle size.}$$

$$⑤ \text{Normal Depth} : y_0 = y_n$$

* Most Economical Channel Section:-

① Rectangular Section:-

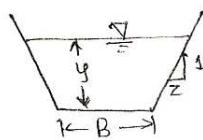
$$R = y/2$$

$$y = B/2$$

② Trapezoidal Section:-

$$R = y/2$$

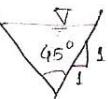
$$\frac{B+2yZ}{2} = y \sqrt{1+z^2}$$



③ Triangular Section:-

$$\theta = 45^\circ \Rightarrow z = 1$$

$$R = \frac{y}{2\sqrt{2}}$$



$$\star \text{Normal Depth for rectangular section} : y_0 = \left[\frac{Q \cdot n}{\sqrt{S_0}} \right]^{3/5} \rightarrow \left[Q = \frac{C}{B} \right]$$

* Computational Problem:-

Basic Eqn : ① 1D continuity Eqn ② Uniform flow formulae / Resistance Eqn
 $Q = A_1 V_1 = A_2 V_2 \quad V = C \sqrt{R S_0}; \quad V = \frac{1}{n} R^{2/3} S_0^{1/2}$

$$\star \text{Conveyance factor} : (K) = \frac{1}{n} A \cdot R^{2/3} = \frac{Q}{\sqrt{S_0}}$$

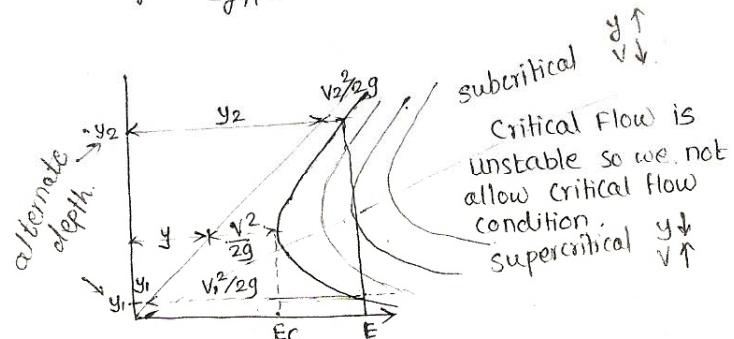
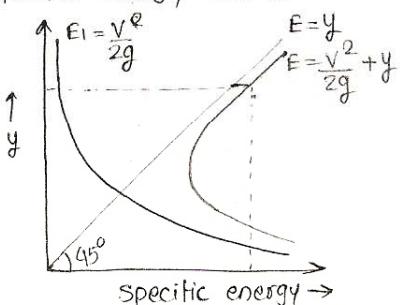
* Specific Energy:-

$$\text{Total energy} = z + \frac{P}{\gamma} + \frac{V^2}{2g} = \text{Datum head} + \text{Pre. head} + \text{Vel. head} \quad (\text{m}) \quad (\text{Nm/N})$$

Specific energy is energy per unit wt. measured w.r.t. channel bed.

$$\Rightarrow S = \frac{P}{\gamma} + \frac{V^2}{2g} \quad (\text{Nm/N}) = \frac{P}{\gamma} + \frac{Q^2}{2g A^2}$$

* Specific Energy Curve:-



Critical flow :- for a given discharge flow at min sp. energy.

$$\text{Froude No} : F = \frac{V}{\sqrt{g D}} = \frac{\text{Inertia Force}}{\text{Gravity Force}} = \frac{\text{Velocity of Flow}}{c = \text{celerity of wave}}$$

$F = 1$ critical
 $F < 1$ subcritical
 $F > 1$ supercritical

If stone is drop on water, waves are moving in all directⁿ is up stream side also, i.e. flow is subcritical. If waves are not seen on upstream side (i.e. vel. is more & depth is less) flow is supercritical.

Critical Flow Condition:-

- ① $F = \frac{V}{\sqrt{gD}} = 1$
- ② $\frac{Q^2}{g} = \frac{A^3}{T}$
- ③ $\frac{V^2}{2g} = \frac{D}{2}$

For wide rectangular channel: (2)

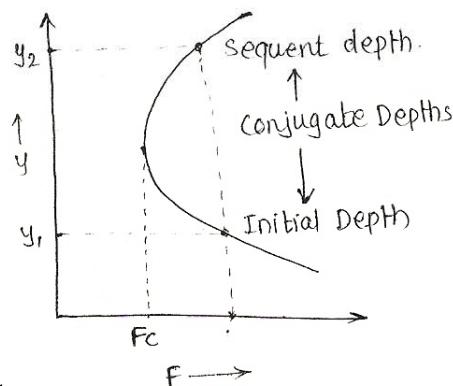
$$D = \frac{A}{T} \approx y$$

$$R = \frac{A}{P} \approx y$$

- ④ For given Sp. energy Discharge is max.
- ⑤ For given discharge Sp. energy is min.
- ⑥ For given discharge, Sp. force is min.

* Specific Force: Force per unit wt. of water.

$$F = \frac{Q^2}{g \cdot A} + A \bar{z}$$



* Critical flow calculations for Rectangular section:

$$y_c = \left[\frac{q^2}{g} \right]^{1/3} \quad y_n = \left(\frac{q \cdot n}{\sqrt{s_0}} \right)^{3/5} \quad E = \frac{3}{2} y_c$$

② Triangular Section:-

$$y_c = \left[\frac{2Q^2}{g \cdot m^2} \right]^{1/5} ; E = 1.25 y_c$$

V. Imp Channel Transition:-

- ① Depth transition
- ② Width transition.

Necessity:-

- ① As reduced discharge causes reduced dim.
- ② Practical difficulties.
- ③ To flume the channel to critical flow.

Types of flume: 1) Venturi flume
2) Standing wave flume
3) Parshall flume } Discharge measuring devices in channel.

① Venturi flume: Depth const. $Q = k \cdot A \alpha \sqrt{2g} (\sqrt{H-h})$

② Standing Wave flume: Depth & width transition. $Q = c \cdot b \cdot H^{3/2}$

③ Parshall flume: Width transition $Q = c \cdot b \cdot H^n$

Velocity measuring devices:-

- ① Pitot tube
- ② current meter \rightarrow cup type
- ③ Propeller type
- ④ Floats.

} Moving boat technique.

Gradually Varied Flow:- (GVF)

① Dynamic eqⁿ GVF, $\frac{dy}{dx} = \frac{S_0 - S_f}{1 - F^2}$ Where, $\frac{dy}{dx}$ = slope of water surface
 S_0 = Bed slope
 S_f = slope of Energy line.
 F = Froude's No.

$$= \frac{S_0 - S_f}{1 - \left(\frac{Q^2 T}{g A^3} \right)}$$

② Dynamic eqⁿ of GVF for wide rectangular channel:-

$$\frac{dy}{dx} = S_0 \cdot \left[\frac{1 - \left(\frac{y_n}{y} \right)^{10/3}}{1 - \left(\frac{y_c}{y} \right)^3} \right] \rightarrow \text{Derived from Manning's eq}$$

$$= S_0 \left[\frac{1 - \left(\frac{y_n}{y} \right)^3}{1 - \left(\frac{y_c}{y} \right)^3} \right] \rightarrow \text{Using Chezy's Eq}$$

$$y_c = \left(\frac{q^2}{g} \right)^{1/3} ; y_n = \left(\frac{q_n}{\sqrt{s_0}} \right)^{3/5}$$

* Classification of canal bottom slope:-

- ① Critical Slope : $S_0 = S_c \Rightarrow y_n = y_c$
- ② Mild slope : $S_0 < S_c \Rightarrow y_n > y_c$
- ③ Steep slope : $S_0 > S_c \Rightarrow y_n < y_c$
- ④ Horizontal : $S_0 = 0 \Rightarrow y_n = \infty$
- ⑤ Adverse slope : $S_0 < 0 \Rightarrow y_n = \text{imaginary}$

* Classification of surface profiles:-

- Zone 1 above top line.
- Zone 2 bet' top & middle line
- Zone 3 below middle line.

① Horizontal

$$S_0 = 0 \\ y_n = \infty$$

② Mild Slope

$$S_0 < S_c \\ y_n > y_c$$

③ Steep Slope

$$S_0 > S_c \\ y_n < y_c$$

④ Critical slope

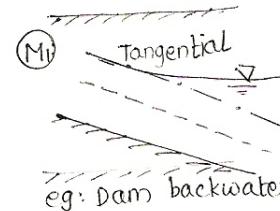
$$S_0 = S_c \\ y_n = y_c$$

⑤ Adverse slope

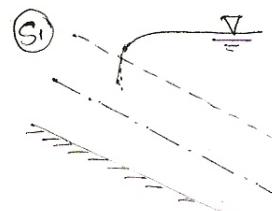
$$S_0 < 0 \\ y_n = \text{Imaginary}$$

above top line.
bet' top & middle line
below middle line.
Zone - 1

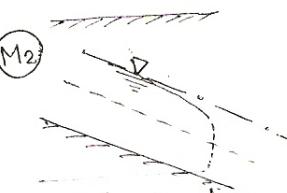
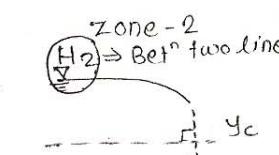
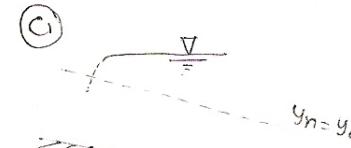
(H1) X → above y_c



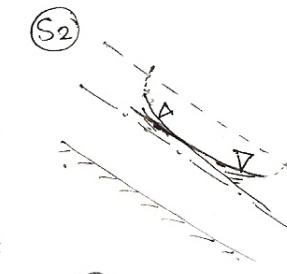
eg: Dam backwater



eg: Meeting of ocean & River



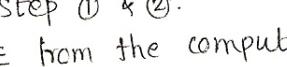
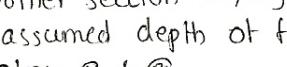
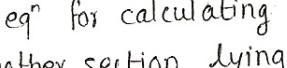
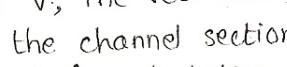
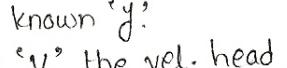
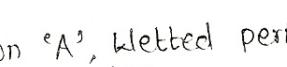
eg: Hydraulic drop



connect



eg: sluice Gate



* Computation of flow profiles:-

- ① Step Mtd.
- ② Graphical integration mtd.
- ③ Direct integration mtd.

① Step Mtd :- Step by step procedure:

- ① Compute area of flow section 'A', wetted perimeter 'P' & hydraulic radius 'R' corresponding to known 'y'.
- ② Compute the mean velocity 'V', the vel. head ($V^2/2g$) & sp. energy 'E', energy line slope 'S_f' at the channel section where 'y' is known. (Use Manning's or chezy's eq for calculating S_f).
- ③ Assume new depth for another section lying very close to the previous one, & from the assumed depth of flow 'y' compute the various quantities as indicated in Step ① & ②.
- ④ Obtain the value of ΔE from the computed values of sp. energies E_1 & E_2 at the two adjacent sections.

(3)

$$\textcircled{5} \quad \overline{Sf} = (Sf_1 + Sf_2) \cdot \dots$$

\textcircled{6} Substitute the values of ΔE , S_0 & \overline{Sf} to compute dx as,

$$dx = \frac{\Delta E}{S_0 - \overline{Sf}} \quad \text{which represents the length of the portion of the}$$

surface profile lying bet' two adjacent sections.

\textcircled{7} Repeat the process by assuming diff. values of depths of flow 'y' at the adjacent sections until the reqd. section is reached, at the resulting dx to obtain reqd. length 'x' of the flow profile.

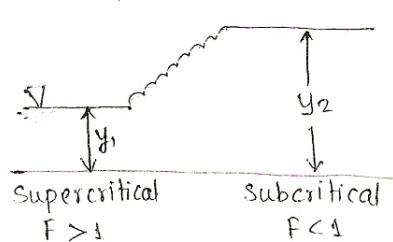
\textcircled{8} Graphical Mtd. of integration:-

$$\frac{dy}{dx} = \frac{S_0 - Sf}{1 - \frac{Q^2 T}{g A^3}} ; \quad dx = f(y) \cdot dy \quad \text{where } f(y) = \frac{1 - \frac{Q^2 T}{g A^3}}{S_0 - Sf}$$

$$\therefore \int dx = \int f(y) dy \Rightarrow (x_2 - x_1) = \int_{y_1}^{y_2} dx = \int_{y_1}^{y_2} f(y) dy$$

\textcircled{9} Direct integration mtd:- (Very complicated)

* Hydraulic Jump :-



[local phenomenon]

y_1 = Pre jump depth / Initial depth

y_2 = Post jump depth / Sequent depth

for rectangular channel,

$$\frac{y_2}{y_1} = \frac{1}{2} [-1 + \sqrt{1 + 8 F_1^2}]$$

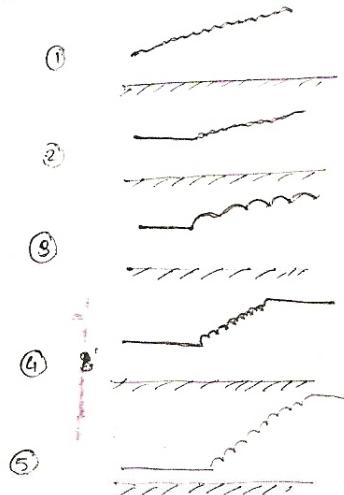
$$\frac{y_1}{y_2} = \frac{1}{2} [-1 + \sqrt{1 + 8 F_2^2}]$$

$$\Delta E = \frac{(y_2 - y_1)^3}{4 y_1 y_2}$$

$$h_j = y_2 - y_1$$

$$L_j = (5 \text{ to } 7 \text{ times}) h_j$$

Types of Jumps:-



undular $F_1 = 1 \text{ to } 1.7$

weak $F_1 = 1.7 \text{ to } 2.5$

oscillating $F_1 = 2.5 \text{ to } 4.5$

steady $F_1 = 4.5 \text{ to } 9$

strong $F_1 > 9.0$

Uses of Jump:-

- \textcircled{1} Energy Dissipation.
- \textcircled{2} Increasing WL in irrigat' channels.
- \textcircled{3} To increase wt. of on apron.
- \textcircled{4} To increase discharge thr' sluice
- \textcircled{5} Mixing chemicals in water & other liquids.