

Notes by-

Pravin S Kolhe,

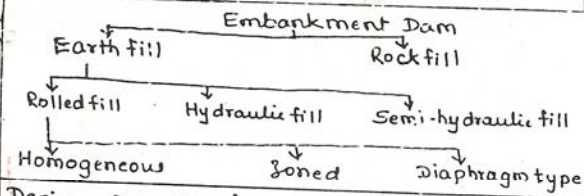
BE(Civil), Gold Medal, MTech (IIT-K)

Assistant Executive Engineer,

Water Resources Department,

www.pravinkolhe.com

Earthen/Embankment Dam



Design of Earthen Dam

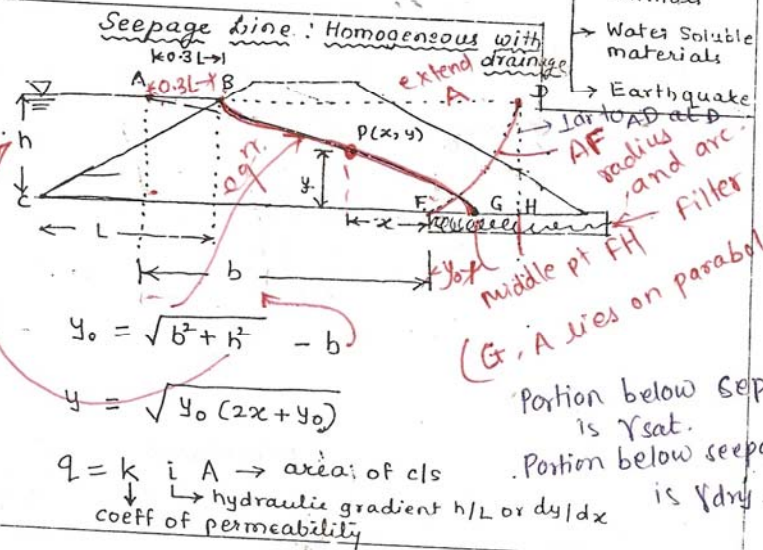
- Crest width :- minimum 3m
Generally 6-12m
- Side Slopes :- 2:1 to 4:1
weak foundation flatter than 4:1
strong foundation greater than 2:1
- Free Board :- $1.5 h_w + \text{safety factor } (0.6-3)$
- Settlement allowance - $1/2 - 2\%$ Height of dam.

Criteria for safe Design :-

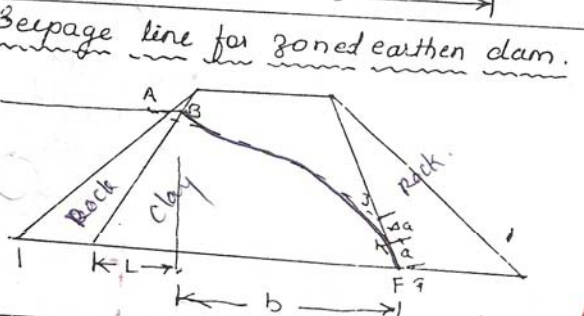
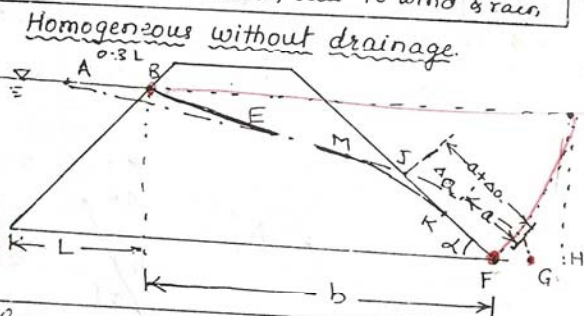
- 1) Safety against overtopping during floods
- 2) Seepage line within the section
- 3) ups & d/s section safe for critical condition
- 4) Foundation safe for shear stresses
- 5) No free passage from ups to d/s
- 6) Dam & foundation safe for piping
- 7) ups slope protected against erosion & wave action.
- 8) d/s slope - erosion due to wind & rain

Causes of failure of earthen dam

- Hydraulic failure**
 - Overtopping
 - Erosion of ups slope by waves
 - Erosion of d/s slope by wind & rain
 - Erosion of d/s toe.
- Seepage failure**
 - Piping through dam & its foundation
 - Conduit leakage
 - Sloughing
- Structural failures**
 - Sliding of ups & d/s slope
 - Slides due to spontaneous liquifaction
 - Burrowing animals
 - Water Soluble materials
 - Earthquake



$q = k i A \rightarrow$ area of c/s
hydraulic gradient h/L or dy/dx
coeff of permeability



D/s and ups portion for horizontal shear

$$S_d = \left[\frac{\gamma H^2}{2bd} \tan^2(45^\circ - \frac{\phi}{2}) + \frac{\gamma_w h_1^2}{2bd} \right] = \frac{H_d}{bd} \rightarrow \text{d/s}$$

$$S_{md} = 2 S_d \quad \text{and} \quad R_d = W_{ed} \tan \phi + c_{bd}$$

$$H_d = \left[\frac{\gamma H^2}{2} \tan^2(45^\circ - \frac{\phi}{2}) + \frac{\gamma_w h_1^2}{2} \right] \leftarrow \text{Imp.}$$

$$F_d = \frac{R_d}{H_d} \geq 2$$

Similarly for ups side.

$$F_u = \frac{R_u}{H_u} \geq 2$$

$$(a + \Delta a) = \frac{y_0}{(1 - \cos \alpha)} \rightarrow y_0 = \sqrt{b^2 + h^2} - b$$

α	$\Delta a / (a + \Delta a)$
30°	0.36
60°	0.32
90°	0.26
120°	0.18
135°	0.14
150°	0.10
180°	0.0

Δa can be found by above eqn & table.

Stability of Earthen Dam

- 1) Against headwater pressure $F_s = \frac{W \tan \phi}{H} > 2$
- 2) D/s and ups portion against horizontal shear
- 3) Foundation of earthen dam against horizontal shear
- 4) Stability of side slopes.
 - (1) ups slope for sudden drawdown
 - (2) (d/s) slope for steady seepage
 - (3) ups & d/s slopes immediately after construction

$$H_u = \frac{\gamma_s H^2}{2} \tan^2(45^\circ - \frac{\phi}{2}) + \frac{\gamma_w h_1^2}{2}$$

$$S_u = \frac{H_u}{b_u}, \quad S_{mu} = 2 S_u$$

$$R_u = W_{eu} \tan \phi + c_{bu}$$

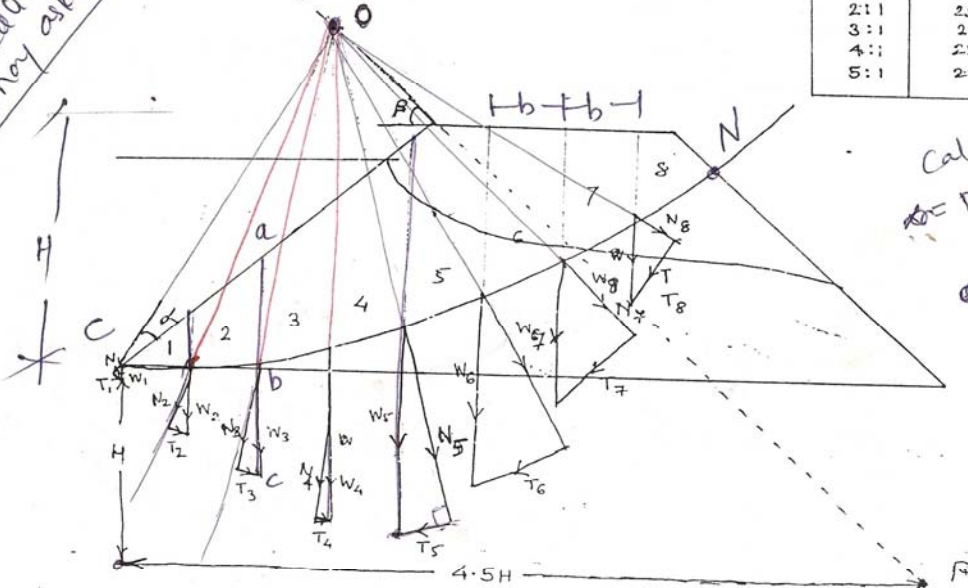
$$F_u = \frac{R_u}{H_u} > 2$$

$$F_{um} = \frac{\text{unit shear stth. at the pt of max. shear stress}}{S_{mu}}$$

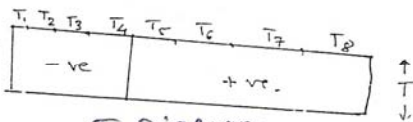
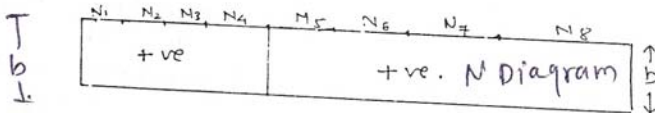
⑦ stability of slide slopes:-

Slope	Directional Angles
0.58:1	23° 40'
1:1	27° 30'
1.5:1	26° 35'
2:1	25° 35'
3:1	25° 36'
4:1	25° 37'
5:1	25° 37'

Procedure may asked



Calculate α & β .
 Draw α & β at shown both meet at O.
 From O go H dist. below from H take 4.5H at P.
 Join OP.
 OP is line on which centre of slip circle lies beyond O.
 O as centre & OC as radius draw arc which is line on which slip of mass occurs.



T Diagram.

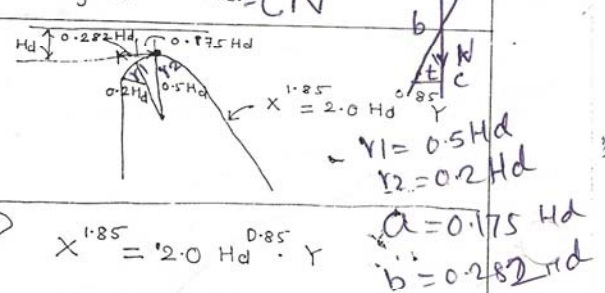
Pro. Asked $F_s = \frac{\sum (N - U) \tan \phi + cS}{\sum T}$

$\sum N = \text{Area of N dia} \times Y$
 & Divide this area in diff. slice of equal width. From O joint bottom pt as shown real & extend them.

$\sum T = \text{Area of T dia} \times Y$ $\times ab = bc$

$\sum N$ - sum of normal components
 $\sum T$ - " " tangential "
 $\sum U$ - " " Pore pressure."
 C - cohesion resistance
 S - length of the arc = CN

- Spillway
- Base on Time of operation :- Main, Auxiliary, Emergency
 - Based on control of flow -> Gated, Ungated
 - Prominent Features:
 - Free overfall
 - Ogee / Diverflow
 - Chute / Open channel / Trough
 - Side channel
 - Morning Glory / Shaft
 - Conduit / Tunnel
 - Siphon



$X^{1.85} = 2.0 Hd^{0.85} \cdot Y$
 $V = \sqrt{2g(Z + H_1 - y)}$
 Z - fall, H_1 - vel. of app. head, y - Tail water depth

Energy Dissipators:-

- $F_1 = 1.7$ to 2.5 - Horizontal apron
 - $F_1 = 2.5$ to 4.5 Type I stilling basin
 - $F_1 > 4.5$ $V_1 < 15$ m/s Type II Stilling Basin
 - $V_2 > 15$ m/s Type III Stilling Basin
- USBR Stilling Basins.

2) $Q = C L H_e^{3/2}$ ungated
 $Q = \frac{2}{3} C_d \sqrt{2g} L (H_1^{3/2} - H_2^{3/2})$

- Indian Standard Stilling Basins
- JHC coincides TWC - Stilling Basin With Horizontal Apron.
 - $F_1 < 4.5$ - Type I IS: Stilling Basin
 - $F_1 > 4.5$ - Type II " " "
 - TWC above JHC for all discharges - IS: Type III
 - TWC above JHC @ large, TWC below JHC when Q small - IS: Type IV.

3) $L = L' - 2(NK_p - K_a) H_e$
 L' - effective length, N - no. of piers, K_p - constant

