

# Theory of Structures

Notes by-

**Pravin S Kolhe,**

BE(Civil), Gold Medal, MTech (IIT-K)

**Assistant Executive Engineer,**

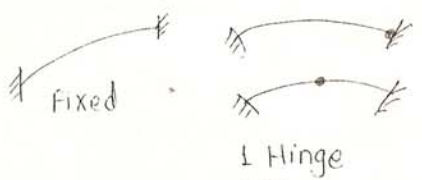
**Water Resources Department,**

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g112 TUS-D  
Types of arches:-

Arches

Date: 06/12/2009

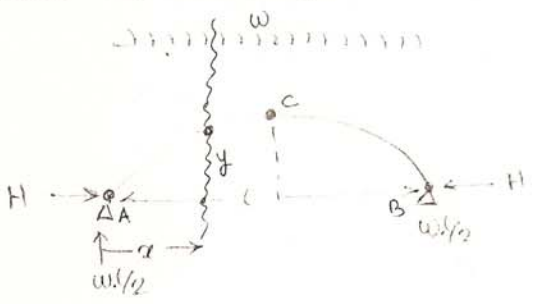


2 Hinge  
Indeterminate  
Dsi = 1

3 Hinge  
Determinate  
Dsi = 0

Shapes:- Parabolic, Circular, elliptical

Imp: Show that the 2hinge arch shown subjected to no BM anywhere on it



Sol<sup>n</sup>:  $\sum F_y = 0$   
 $\therefore R_A + R_B = w \cdot l$   
 $\therefore R_A = R_B = w \cdot l / 2$

$\sum M_c = 0$   
 $w \cdot l / 2 \times \frac{l}{2} = H \cdot h + \frac{w \cdot l}{2} \cdot \frac{l}{4}$

$H = \frac{w \cdot l^2 \cdot h}{8h}$

 $\therefore H = \frac{w \cdot l^2 - \frac{w \cdot l^2}{3}}{4h}$ 

$H = \frac{w \cdot l^2 \cdot h}{8h}$

To show that BM at any section is zero,

$\sum M_{x-x} = 0$

$\sum M_x = w \cdot \frac{l}{2} \cdot x - H \cdot y - w \cdot \frac{x^2}{2}$

$= w \cdot \frac{l}{2} \cdot x - H \cdot \left( \frac{4hx}{l^2} \right) x(l-x) - w \cdot \frac{x^2}{2}$

$= w \cdot \frac{l}{2} \cdot x - \frac{w \cdot x^2}{2} (l-x) - w \cdot \frac{x^2}{2}$

$= w \cdot \frac{l}{2} \cdot x - \frac{w \cdot x^2 \cdot l}{2} + \frac{w \cdot x^3}{2} - \frac{w \cdot x^2}{2}$

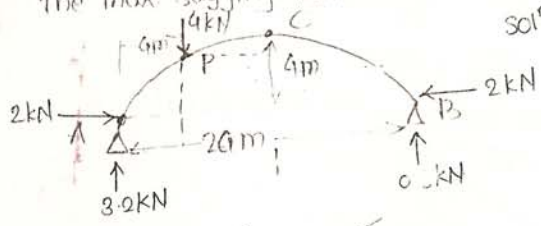
& Eq<sup>n</sup> of parabola is  
 $y = \frac{4hx}{l^2} (l-x)$

$M_x = 0$

Note: The BM is zero for arch carrying udl on its entire span, irrespective of support levels, for 3H arch only.

Imp V.V. Imp

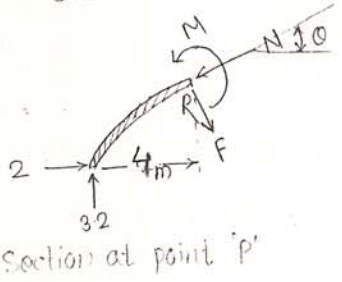
find the thrust, radial shear, and bending moment at 'P'. Also find the max sagging moment & hogging moments on the arch.



Sol<sup>n</sup>:  $R_B \times 20 = 4 \times 4$   
 $\therefore R_B = 0.8 \text{ kN}$

$R_A \times 20 = 4 \times 16$   
 $\therefore R_A = 3.2 \text{ kN}$

$\sum M_c = 0$   
 $H \times 4 + 4 \times 6 = 3.2 \times 10$   
 $\therefore H = 2 \text{ kN}$



$\tan \theta = \frac{dy}{dx} = \frac{4h}{l^2} (l-2x)$

$= \frac{4 \times 4}{(20)^2} (20-8)$

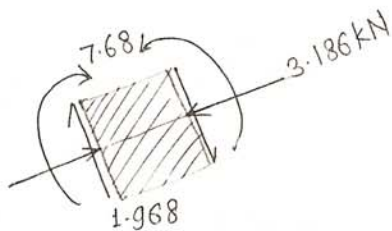
$\therefore \theta = 25.64^\circ$

03/12/2009

Influence line Diagram

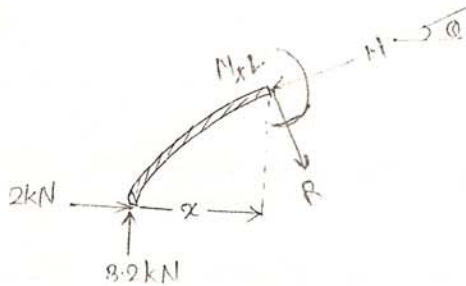
$$\begin{aligned} \sum F_x &= 0 \\ 2 + R \sin \theta &= N \cos \theta \Rightarrow N \cos \theta - R \sin \theta = 2 \\ 3.2 &= N \sin \theta + R \cos \theta \Rightarrow N \sin \theta + R \cos \theta = 3.2 \\ R &= 1.966 = 2.021 \\ N &= 3.22 = 3.186 \end{aligned}$$

$$\begin{aligned} \sum M_P &= 0 \\ M + 2(y_p) - 3.2(4) &= 0 \\ M + 2 \left[ \frac{4h}{x^2} \cdot x(1-x) \right] - 3.2 \times 4 &= 0 \\ M + 2 \left[ \frac{4 \times 4}{20^2} \times 4(20-4) \right] - 3.2 \times 4 &= 0 \\ \boxed{M = +7.68 \text{ kNm}} \end{aligned}$$



The element at 'p' (without considering 4kN)

We now go on to the BMD of arch



$$\begin{aligned} M_x &= 3.2x - 2y \quad \left( \frac{4h}{x^2} \cdot x(1-x) \right) \text{ for } \tan \theta \text{ or derivative} \\ M_x &= 3.2x - \frac{2 \times 4 \times 4}{400} \cdot x(20-x) \\ M_x &= 3.2x - \frac{x(20-x)}{12.5} \quad \text{at } x=0, M_0 = 7.68 \text{ kNm} \end{aligned}$$

i.e. BM

$$\frac{dM}{dx} = 3.2 - \frac{1}{12.5} [20 - 2x]$$

at  $x=0$ ,  $\frac{dM}{dx} = +1.6$  i.e. +ve slope

$$\frac{d^2M}{dx^2} = \frac{2}{12.5} \text{ (+ve)}$$

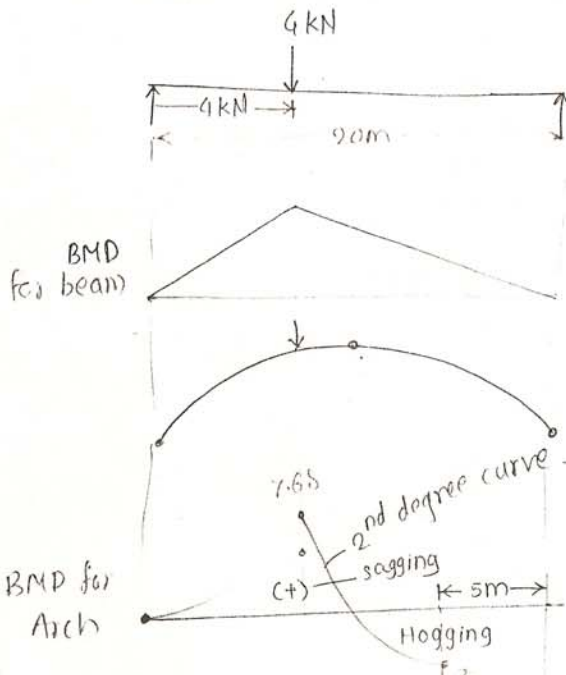
Means rate at which 1<sup>st</sup> derivative changes

is +ve. ①

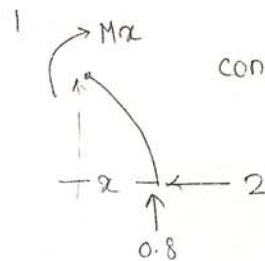
i.e.



∴ 2<sup>nd</sup> curve is correct.



∴ M<sub>sagging</sub> max = 7.68 kNm ... at  $x=16$   
 M<sub>Hogging</sub> max = -2 kNm at  $x=5$

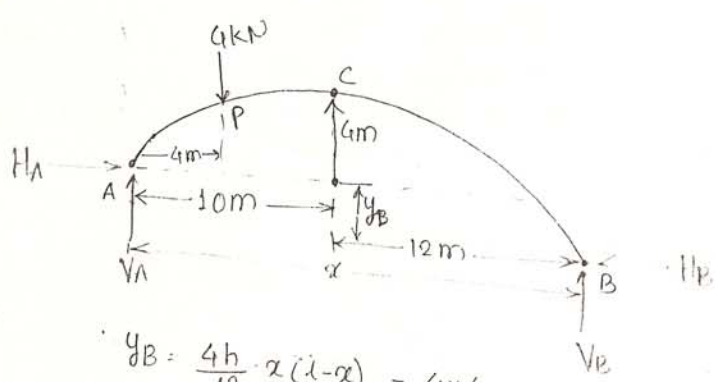


considering Right part

$$\begin{aligned} M_x &= 0.8x - 2y \\ &= 0.8x - \frac{4 \times 4 \times 2 \times (20-x)}{400} \end{aligned}$$

limits 0 to 16

$$\begin{aligned} M_x &= 0.8x - 0.08(20-x) \cdot x \\ \text{at } x=0, M_0 &= 0 \\ x=10, M_{10} &= 0 \\ x=16, M_{16} &= 7.68 \end{aligned}$$



$$y_B = \frac{4h}{l^2} \cdot x(l-x) = \frac{4 \times 4}{20^2} \times 22(20-22) = -1.76 \text{ m.}$$

Assuming  $h=4\text{m}$ ,  $x=22\text{m}$

$$\sum M_B = 0$$

$$\therefore V_A(22) = H_A(1.76) + 4(18) \Rightarrow 22V_A - 1.76H_A = 72$$

$$\sum M_C = 0$$

$$\therefore H_A(4) + 4(6) = V_A(10) \Rightarrow 10V_A - 4H_A = +24$$

$$\therefore V_A = 3.49 \text{ kN}$$

$$H_A = H_B = 2.727 \text{ kN}$$

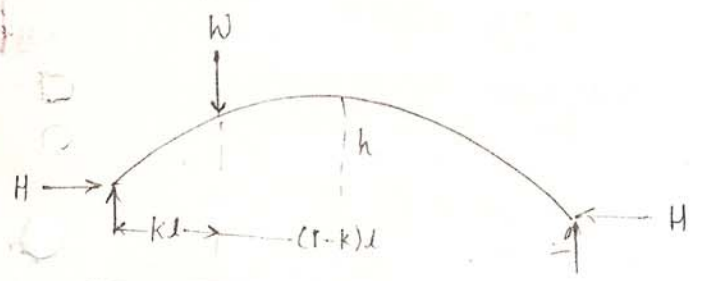
Then  $\sum M_A = 0$

$$\therefore 22V_B - 1.76H_B - 4 \times 4 = 0$$

$$V_B = 0.945 \text{ kN}$$

To find BM, consider section just left to 'P' & then upto 'B'.

Two Hinge Arch

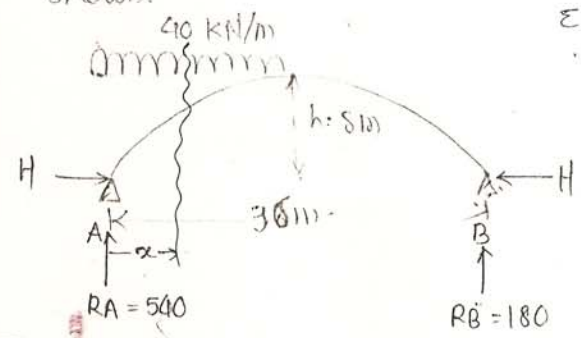


$$H = \frac{5}{8} \frac{W \cdot l}{h} (k - 2k^3 + k^4)$$

v. Imp. or  $H = \frac{5}{8} \frac{W \cdot k}{h} (1 - 2k^2 + k^3)$

If udl acts on arch

Q: Determine the position & magnitude of the max BM for the arch shown.



$$\sum M_A = 0$$

$$\therefore 36R_B = 40 \times 18 \times 9$$

$$\therefore R_B = 180 \text{ kN.}$$

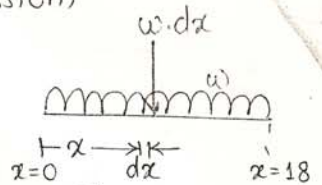
$$R_A = 540 \text{ kN}$$



Horizontal reaction is obtained by from the basic expression,

i.e.  $H = \frac{5\omega l k}{8h} (1 - 2k^2 + k^3)$

Integrating in the tributary length in the udl.



$\therefore dH = \frac{5}{8} \frac{\omega dx \cdot l}{h} (k - 2k^3 + k^4)$  where  $k = \frac{x}{l} \rightarrow$  limits.

$\therefore x = kl$

$dH = \int_0^{0.5} \frac{5}{8} \frac{\omega \cdot l \cdot dk \cdot l}{h} (k - 2k^3 + k^4)$  It's better to replace dx by dk  
 $\therefore dx = l \cdot dk$

$= \frac{5}{8} \frac{\omega l^2}{h} \int_0^{0.5} (k - 2k^3 + k^4) dk$

$= \frac{5\omega l^2}{8h} \left[ \frac{k^2}{2} - 2\frac{k^4}{4} + \frac{k^5}{5} \right]_0^{0.5} = \frac{5}{8} \frac{\omega l^2}{h} \left[ \frac{(0.5)^2}{2} - 2\frac{(0.5)^4}{4} + \frac{(0.5)^5}{5} \right]$

$= \frac{5\omega l^2}{8h} [0.1]$  ✓

$H = 405 \text{ kN}$

$= \frac{0.5\omega l^2}{8h} \left[ H = \frac{0.5\omega l^2}{8h} \right]$



Consider a section at x from A.

$\therefore M_x = 540x - 40\frac{x^2}{2} - 405 \times y \rightarrow \frac{4h}{l^2} \cdot x(l-x)$   
 $\rightarrow \frac{4 \times 8}{36^2} \times x(36-x)$  ( $0 \leq x \leq 18$ )

$M_0 = 0$   
 $M_{18} = 0$  } Speciality of Half loaded arch with udl  
 with supports are at same level.

Examine the  $f''$ :

$\frac{dM}{dx} = 540 - 40x - 10(36 - 2x) \Rightarrow 540 - 40x - 360 + 20x = 0$

$\frac{d^2M}{dx^2} = -40 - 10(-2) = -20$

i.e. curve starts with +ve slope.

at  $x=0$ ,  $\frac{dM}{dx} = +ve$ .

$\therefore \frac{dM}{dx}$  is zero at  $x=9$   
 i.e. at turning point.

$M_3 = 810 \text{ kNm}$

for RHS :-

$M_x = 180x - 405 \times \frac{4 \times 8}{36^2} \times x(36-x)$

$= 180x - 10x(36-x)$

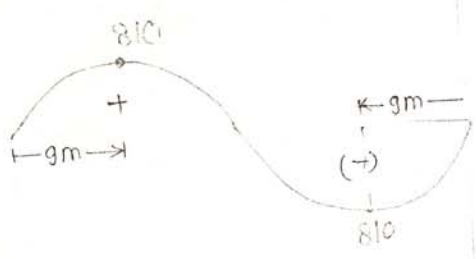
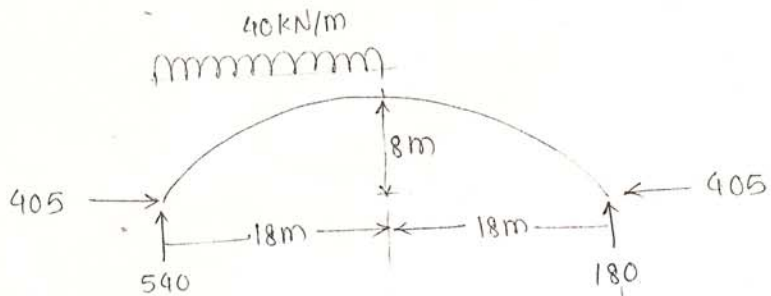
at  $x=0$ ,  $M_x = 0$

at  $x=18$ ,  $M_{18} = 0$

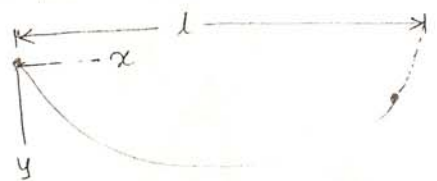
$\frac{dM_x}{dx} = 180 - 360 + 20x = -180 + 20x$

$\frac{d^2M_x}{dx^2} =$

check  $M_g = -810 \text{ kNm}$



[Suspension Cables]



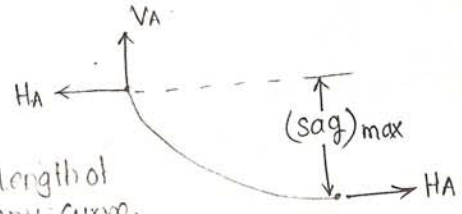
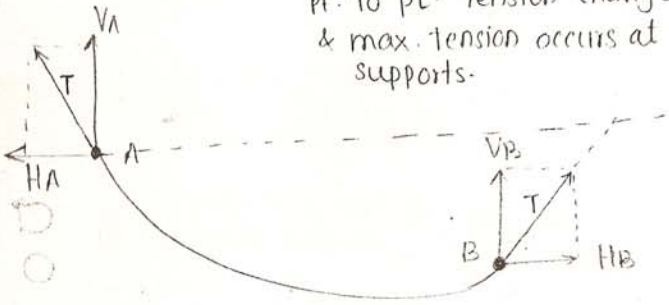
Shape is assumed to be parabolic

Eq<sup>n</sup> of cable,  
 $y = \frac{4h}{l^2} x(l-x)$

- \* No BM
- \* No SF
- \* Only Tension.

Pt. to pt. Tension changes & max. tension occurs at supports.

Max. sag occurs at the pt. where slope is zero.

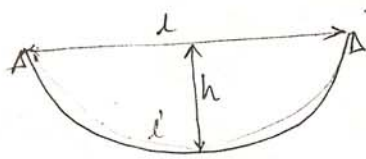


Length of the cable =  $\int \sqrt{1 + \left(\frac{dy}{dx}\right)^2} \cdot dx$

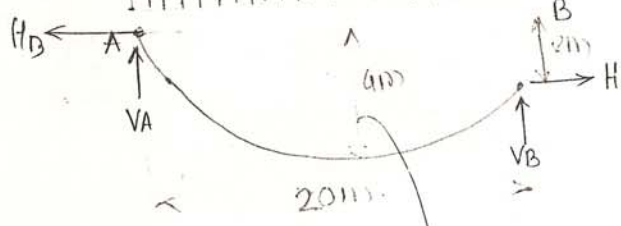
Length of any curve.

Using Binomial expansion we obtain an approx. expression for the length of the cable, supported at the centre.

Prob Find the max. Tension for in the suspended cable loaded as shown. 10 kN/m



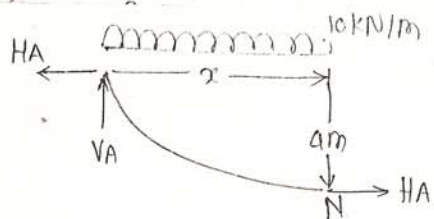
length of Curve =  $l' = l + \frac{8}{3} \frac{h^2}{l}$   
 Parabola.



Sol<sup>n</sup> :-  $\sum M_B = 0$   
 $20VA = 10 \times 20 \times 10 + 2HA$   
 $20VA - 2HA = 2000$

$\sum M_A = 0$   
 $20VB = 10 \times 20 \times 10 + 2HB$   
 $20VB - 2HB = 2000$

4m is not at centre & this can be solved by Mechanics.



$$\sum M_N = 0$$

$$H_A(4) + 10 \frac{x^2}{2} = V_A \cdot x$$

$$\sum F_y = 0$$

$$\boxed{V_A = 10x}$$

$$\therefore H_A(4) + 10 \frac{x^2}{2} = 10x^2$$

$$\therefore H_A = \frac{10x^2 - 10 \frac{x^2}{2}}{4} = \boxed{\frac{5x^2}{4} = H_A = H_B}$$

$$T_{max} = 172 \text{ kN} \sqrt{H_A^2 + V_A^2} \quad \text{solving for 'x', } x = 11.72 \text{ m}$$

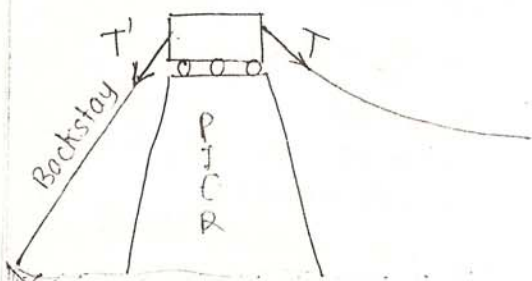
occurs at 'A' . i.e. Higher slope, or max. slope.

$$H_A = 172 \text{ kN} = H_B$$

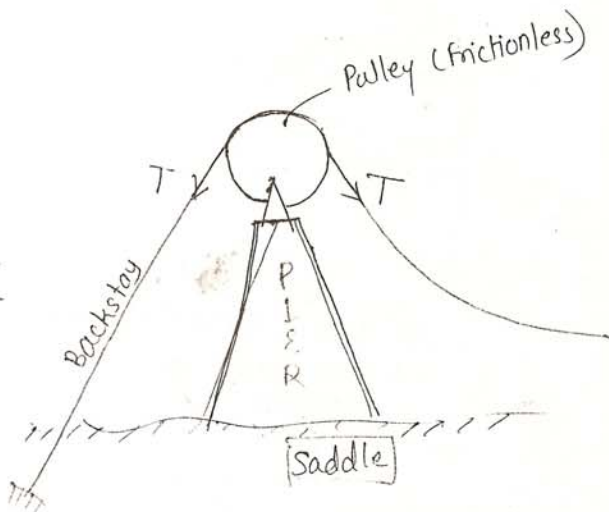
$$V_A = 117.2$$

$$\boxed{T_{max} = 208 \text{ kN}}$$

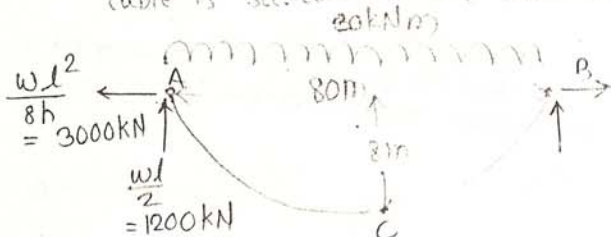
\* Anchorages:



"MPSC" [saddle]

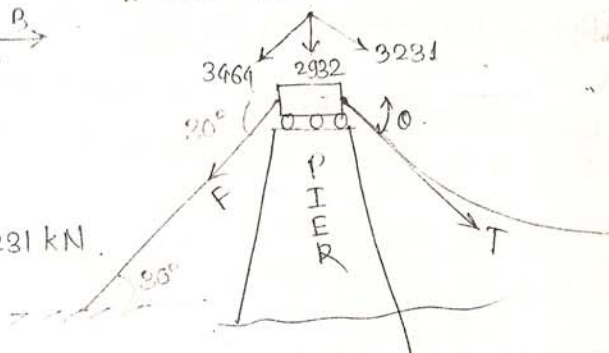


PRO:- Find the tension in the backstay & the pres. on the pier, if the cable is saddle & the backstay is at 30° with the horizontal.



$$\therefore T = \sqrt{1200^2 + 3000^2} = 3231 \text{ kN}$$

To find Reaction take EMC = 0



: Eq<sup>m</sup> condition,

$$F \cos 30 = T \cos(21.8)$$

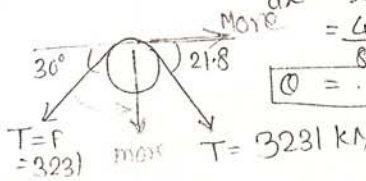
$$\therefore F = \frac{3231 \cos(21.8)}{\cos 30}$$

$$\boxed{F = 3464 \text{ kN}}$$

$$\tan \theta = \frac{dy}{dx} = \frac{4h}{l^2} (1-2x) \quad \text{at } x=0 \quad \text{ie at anchorage}$$

$$= \frac{4 \times 8}{80^2} (80-0)$$

$$\theta = 21.8^\circ$$



Net pressure on pier =  $\sum F_y = 0$

$$F \sin 30 + T \sin(21.8) = 3464 \sin 30 + 3231 \sin(21.8)$$

$$= 2932 \text{ kN}$$

"Saddle" the cable is running over a frictionless pulley & then same angle, then Horizontal force on pier =  $3231 (\cos 21.8 - \cos 30) = 201.8$